

The Interaction of Wind Turbine With Local Network

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The Interaction of Wind Turbine With Local Network

- Network strength (SCL or SCR)
- Voltage variations and flicker
- Harmonics
- Reactive power
- Protection
- Frequency
- Network stability

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System Strength (SCL or SCR)

$$SCR = \frac{SCL}{P_w}, \quad SCL = \frac{U_{sc}^2}{Z_{sc}}$$

SCR : Short Circuit Ratio,
 SCL : Short Circuit Level,
 P_w : Installed wind power,

- Strong system $20 < SCR < 25$
- Weak system $8 < SCR < 10$



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Voltage Variations and Flicker Level

Flicker severity factor	Planning levels		Emission levels
	MV (1-36)	HV (36-230)	MV and HV
P _{st}	0.9	0.8	.35
P _{lt}	0.7	0.6	0.25

$$P_{lt} = \sqrt[3]{\frac{1}{12} \sum_{j=1}^{12} P_{stj}^3}$$

P_{lt} : Long term (2 hours) flicker severity factor,

P_{st} : Short term (10 min.) flicker severity factor,

$\Delta V = 2\%$: Different for networks

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Harmonics

IEC 1000-3-6 Guidelines	Planning levels		Compatibility level
	MV	HV	MV
THD	6.5%	3%	8%

$$THD = 100 \sqrt{\sum_{n=2}^{50} \frac{U_n}{U_1} \%}$$

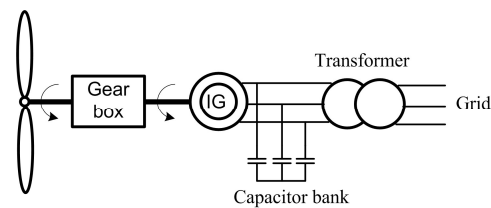
U_n : Individual harmonic amplitude (or RMS) voltage,

U_1 : Fundamental amplitude (or RMS) voltage

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Reactive Power



Fixed speed WTs with an induction generator need reactive power support.

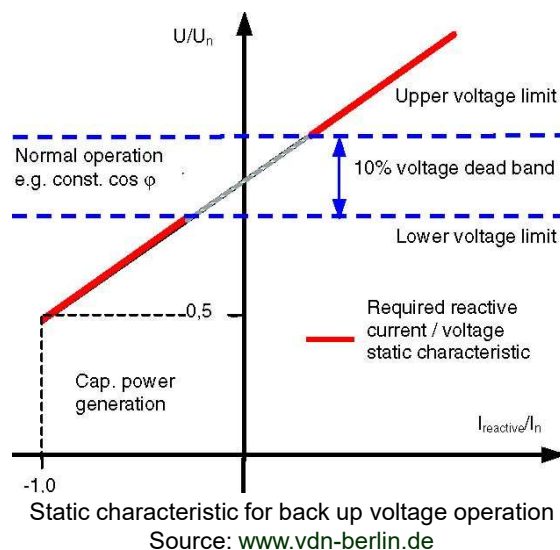
0.9 lagging < p.f. < 0.95 leading, suggestion above 0.96

Variable speed WTs with converter can have unity p.f.

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Reactive Power Support of Network



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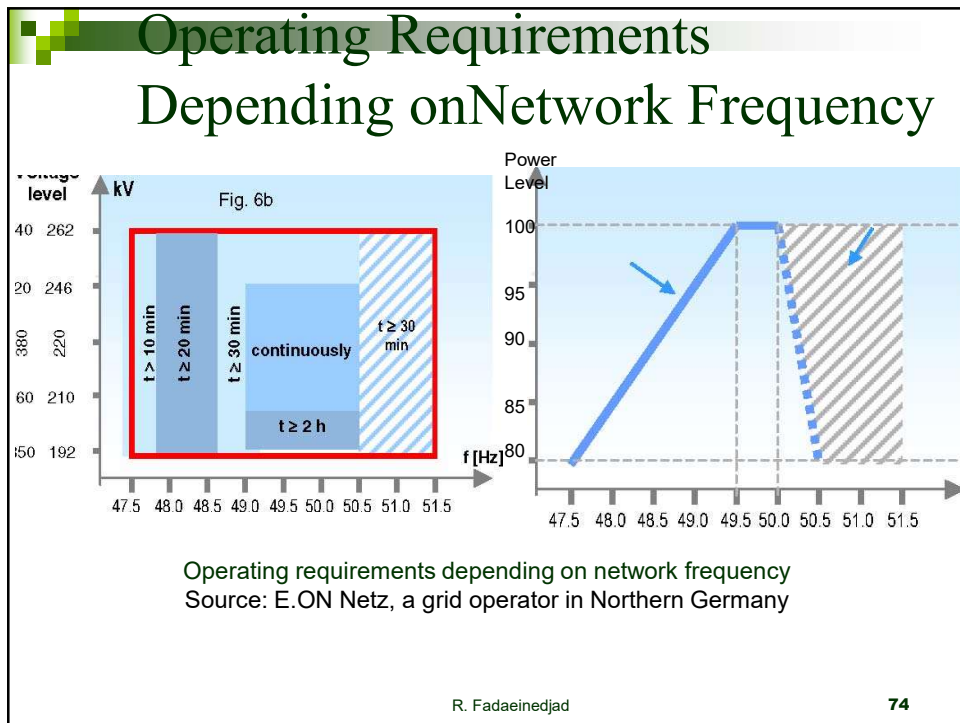
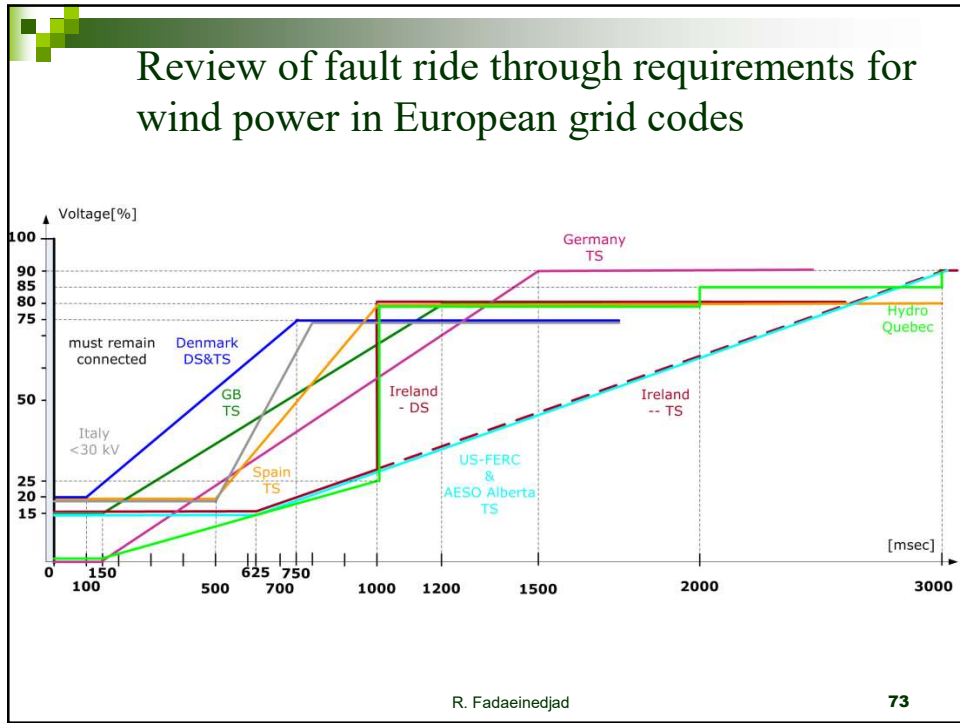
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Required Protection Functions

- Under frequency
- Over voltage
- Under voltage
- Loss of mains
- High over currents
- Thermal overload
- Earth fault
- Neutral voltage displacement
- Rate Of Change Of Frequency (ROCOF) relay for autonomous operation

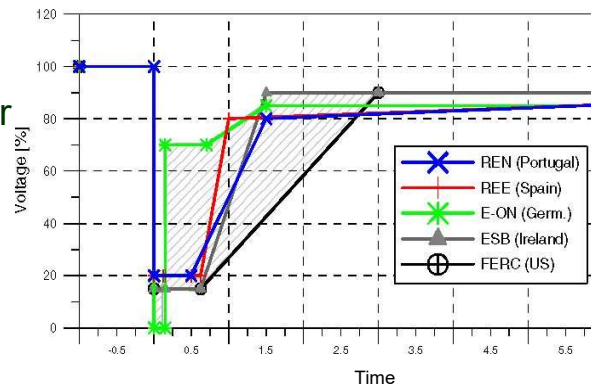
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Fault Ride-Through

- Voltage dip requirements
- The effect of power system voltage dips on both electrical and mechanical parts of wind turbine
- The stability of wind turbine controllers



LVRTF requirements for several grid codes

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Some Guidelines for Grid Connection Considering Power Quality Issue Based on IEC 61400-21 (Calculation Method)

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Steady State Voltage Change by WT

Load flow as the best method:
low (high) loads and low (high) wind power

A simple method:

$$d = \frac{S_{60}}{S_k} |\cos(\psi - \varphi)| \text{ for } \cos(\psi - \varphi) > 0.1 ,$$

S_k : Short circuit Power at PCC,

S_{60} : Apparent power at the 1-min. active power peak,

d : steady state voltage change of the grid at PCC (normalised to nominal voltage),

φ : Phase angle between voltage and current,

ψ : Grid impedance phase angle

Voltage Change Due to Switching Operations of a WT

$$d = K_u(\psi_k) \cdot \frac{S_n}{S_k}$$

S_k : Short circuit Power of grid at PCC,

S_n : Apparent power of WT at rated power,

d : Relative voltage change,

$K_u(\psi_k)$: Voltage change factor,

ψ_k : Grid impedance phase angle at PCC

Flicker Due to Continuous Operation of a Single WT and Multiple WTs

$$P_{lt} = c(\psi_k, v_a) \cdot \frac{S_n}{S_k}$$

S_k : Short circuit Power of grid at PCC,
 S_n : Apparent power of WT at rated power,
 P_{lt} : Flicker distortion,
 $c(\psi_k, v_a)$: Flicker coefficient,
 v_a : Annual average wind speed,
 ψ_k : Grid impedance phase angle at PCC,

$$P_{lt-(nWTs)} = \sqrt{n} \cdot P_{lt-(singleWT)},$$

n : Number of wind turbines

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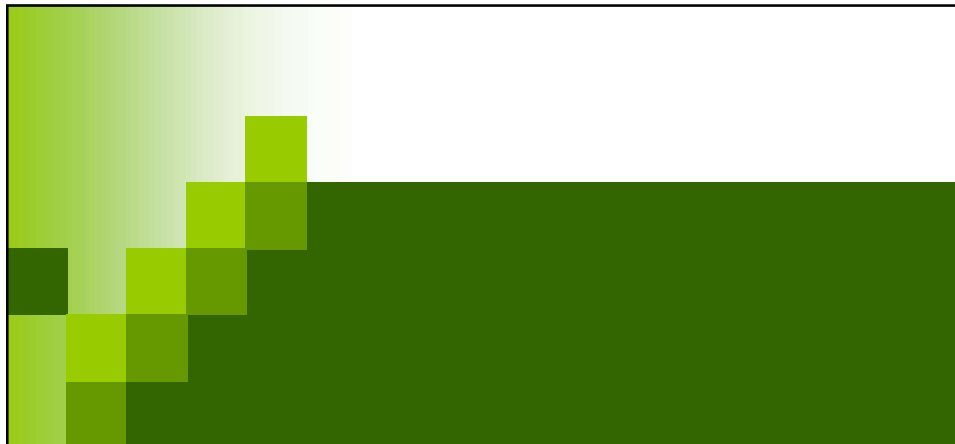
Flicker Due to Switching Operations of a single WT

$$P_{lt} = 8 \cdot N_{120} \cdot K_f(\psi_k) \cdot \frac{S_n}{S_k}$$

S_k : Short circuit Power of grid at PCC,
 S_n : Apparent power of WT at rated power,
 P_{lt} : Flicker distortion,
 $K_f(\psi_k)$: Flicker step factor,
 N_{120} : Number of switching within a 2 hours period,
 ψ_k : Grid impedance phase angle at PCC

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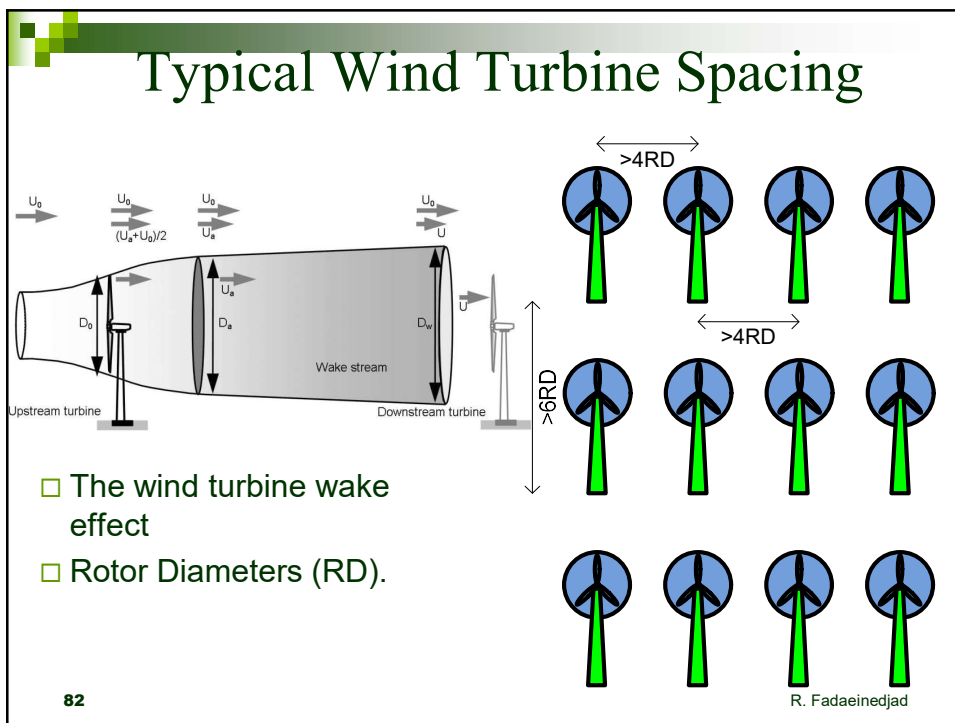
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Flicker Contribution of a Wind Power Plant with Single and Multiple Turbine Representations

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Typical Wind Turbine Spacing



- The wind turbine wake effect
- Rotor Diameters (RD).

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Power Quality and Flicker Issue

- Wind speed fluctuation can cause power variations in a wind power system.
- Flicker and voltage variations are induced by load flow changes in the grid.
- The flicker emission produced by a wind power plant during normal operation is mainly caused by fluctuations in the output power due to wind speed variations, tower shadow effect, and wind shears.

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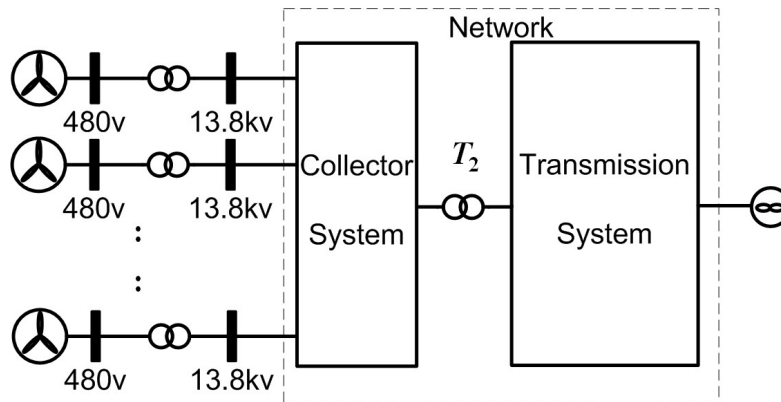
Aeroelastic Issues and Power Quality

- Aerodynamic Issues
 - Wind velocity variations (Stochastic)
 - Wind shear (Periodic)
 - Tower shadow (Periodic)
 - Yaw error (Periodic)
- Mechanical Issues
 - Tower and blades vibration

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System Configuration



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Wind Power Plant

Representations

- Single Turbine Representation (STR)
- Multiple Turbine Representation (MTR)
- Quasi Multiple Turbine Representation (QMTR)

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Single Turbine Representation (STR)

$WTG = 1$

- The WTG units is replaced by an equivalent WTG unit.
- The collector system is represented by an equivalent impedance.
- This is the worst-case assumption and the same wind fluctuations and tower shadow effects will affect the output power of the wind power plant and the power quality at the PCC.

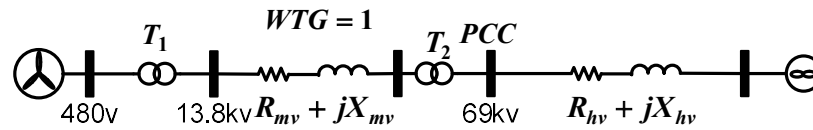
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Multiple Turbine Representation (MTR)

- WTs are divided in several groups and each group is represented by a WT.
- The wind speed file is subdivided into several sections and each subdivision is applied to a different group of WTs.
- WTs should be simultaneously modeled.
- Computational time.
- Still all WTs are not modeled.

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Quasi Multiple Turbine Representation (QMTR)

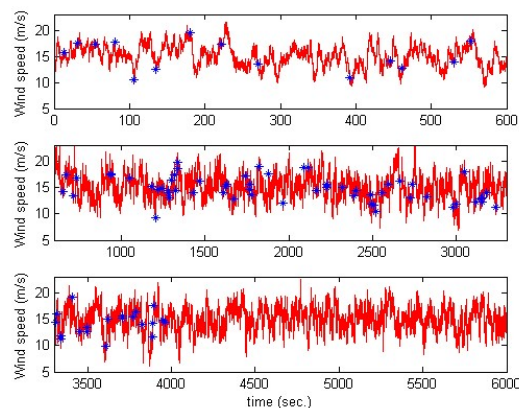


- The STR is used.
- The time series of wind file is subdivided into several sections and are applied to STR of wind farm.
- Considering WTs as independent sources connected to a linear network, the average of the results for the network quantities (i.e. the voltage, active power, and reactive power) at PCC are calculated.

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The Wind Speed Distribution



- The time series of wind speed is divided into 96 different files with the starting times shown by stars (*)

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The Computation Load for QMTR and MTR Methods

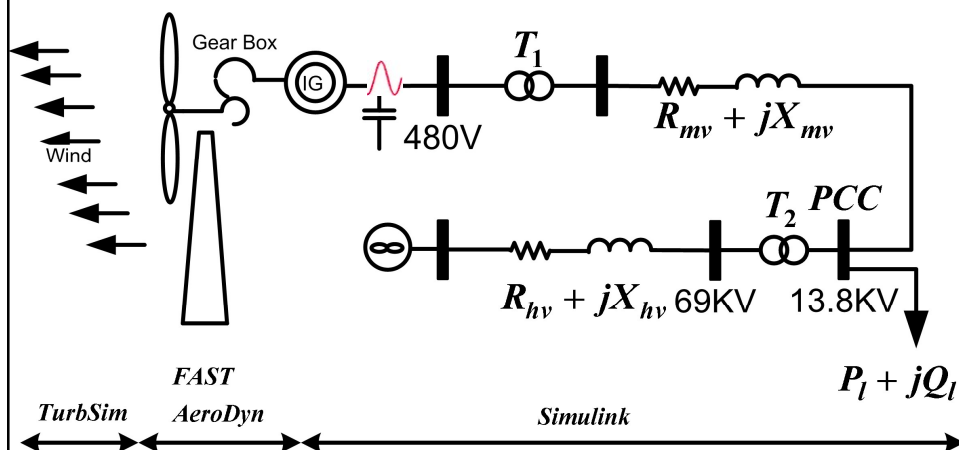
$C_1 = C_{wt} \cdot T_1 + C_{avr}$, $C_2 = N \cdot C_{wt} \cdot T_2$
 C_1, C_2 : Computation loads for QMTR and MTR,
 T_1, T_2 : Simulation times for QMTR and MTR
 N : WTs in wind farm,
 C_{wt} : Computational load of a WT for 1 Sec.,
 C_{avr} : Averaging computation load,

To simulate wind farm for 600 Sec. we have:
 $N = 96$, $T_1 = 600 + 96 \times 60$, $T_2 = 600$, and
 $C_{avr} \approx C_{wt}$ it can be concluded that
 $C_2 \approx 9 \times C_1$.

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Simulation Structure



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Simulation Steps

- Task 1: Simulation of wind and aerodynamic forces using TurbSim and AeroDyn
- Task 2: Simulation of mechanical parts of wind turbine using FAST
- Task 3: Time domain simulation of the induction generator and grid (including transformers, collector system, and transmission system)

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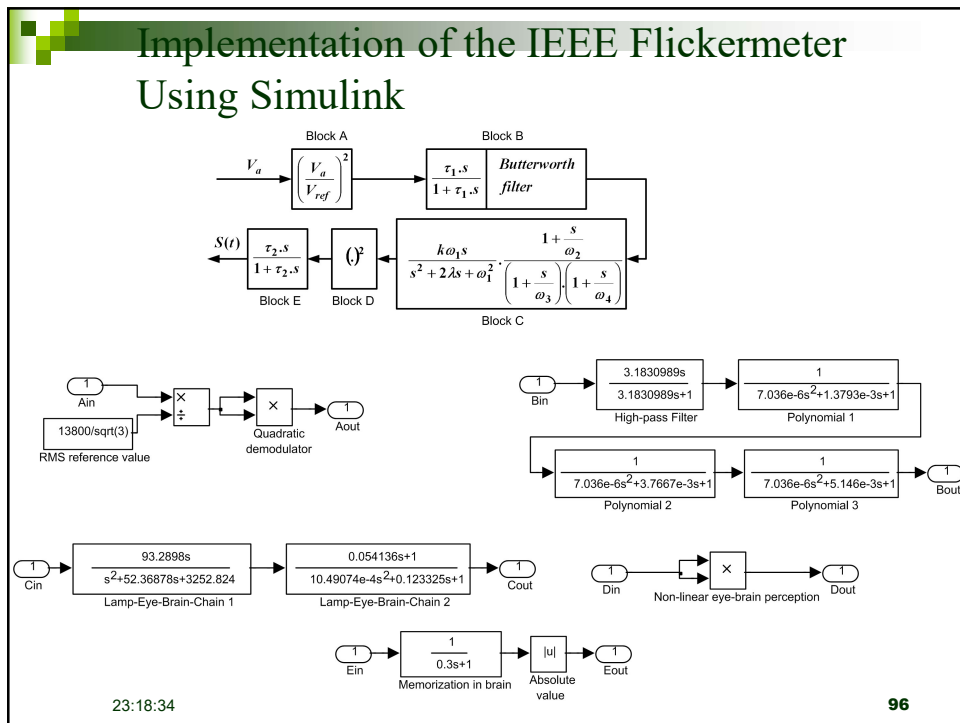
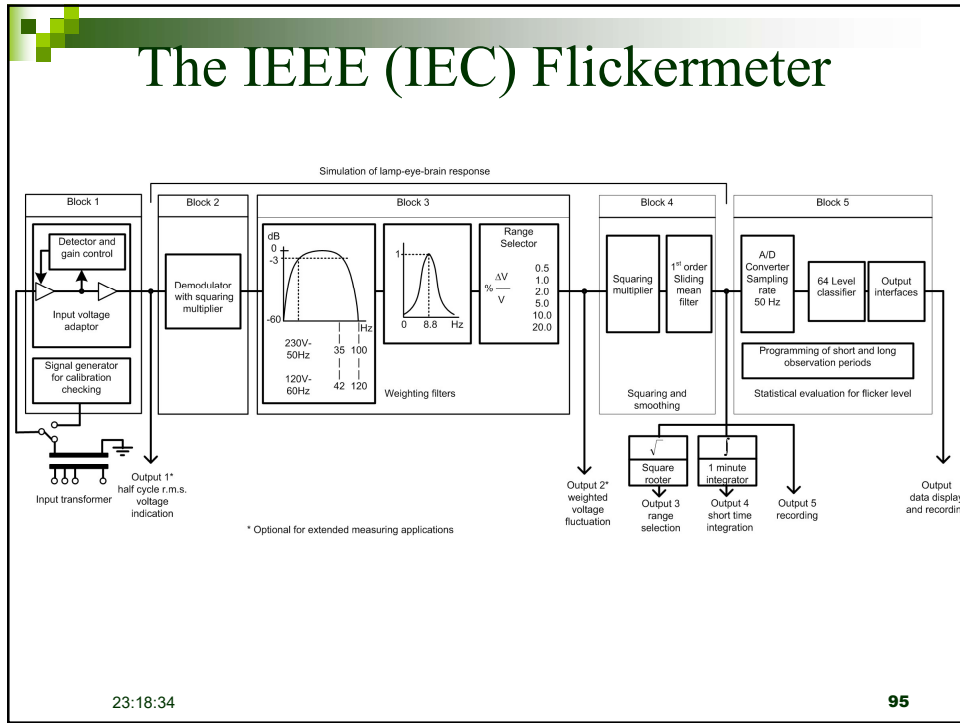
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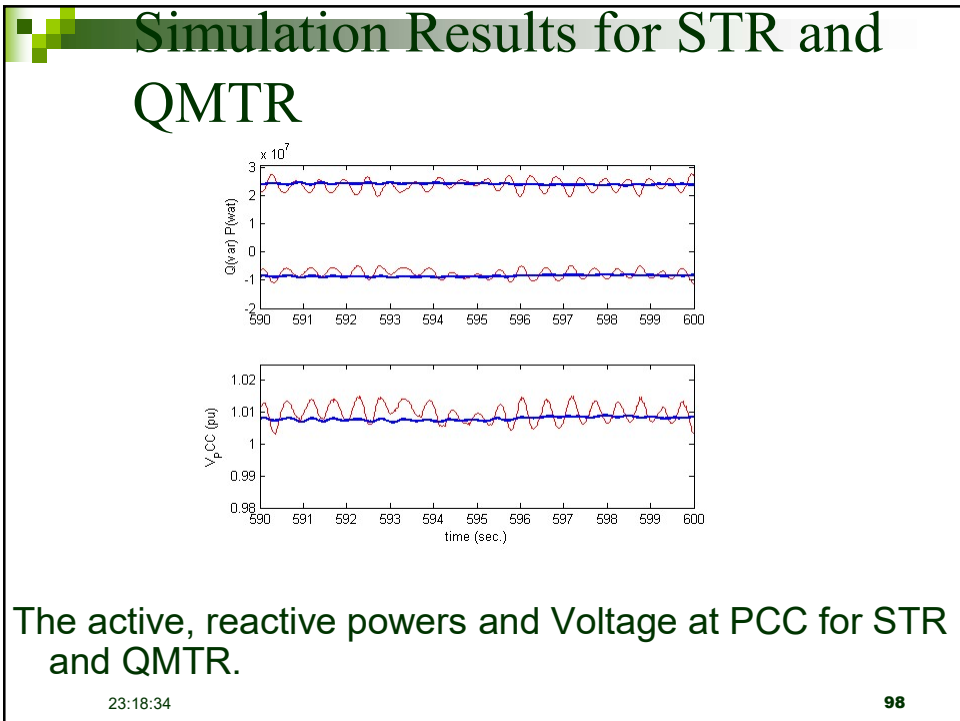
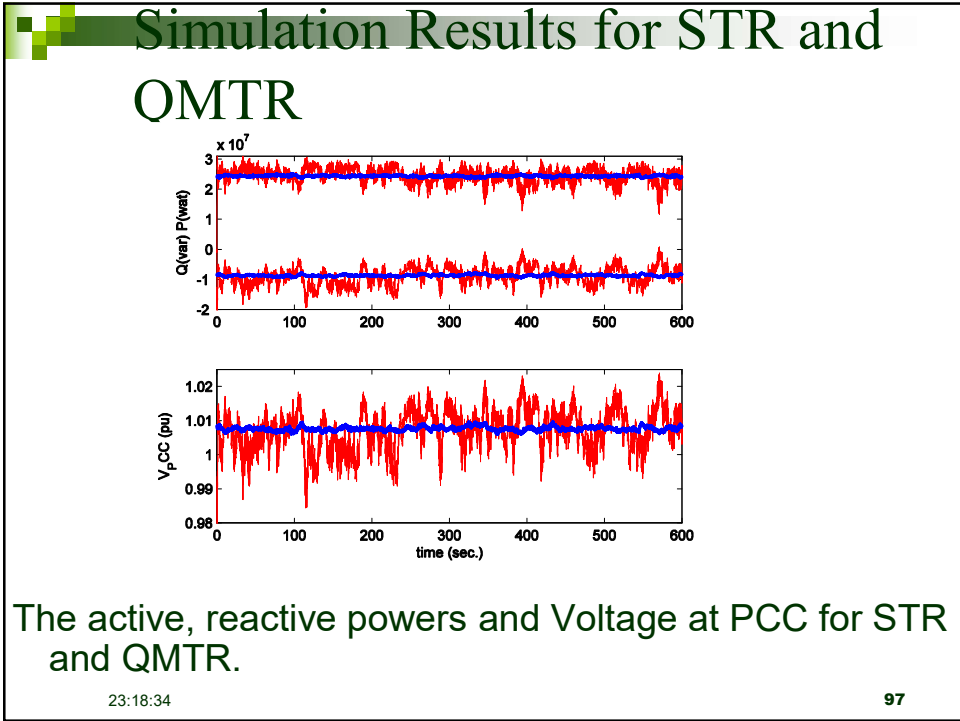
Simulation Steps (contd.)

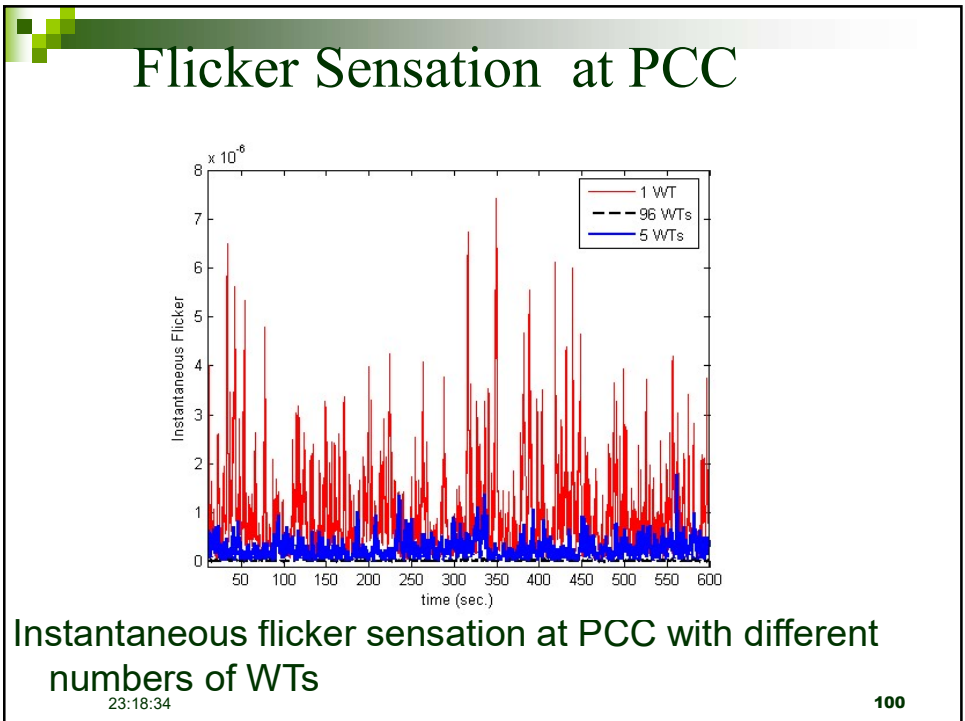
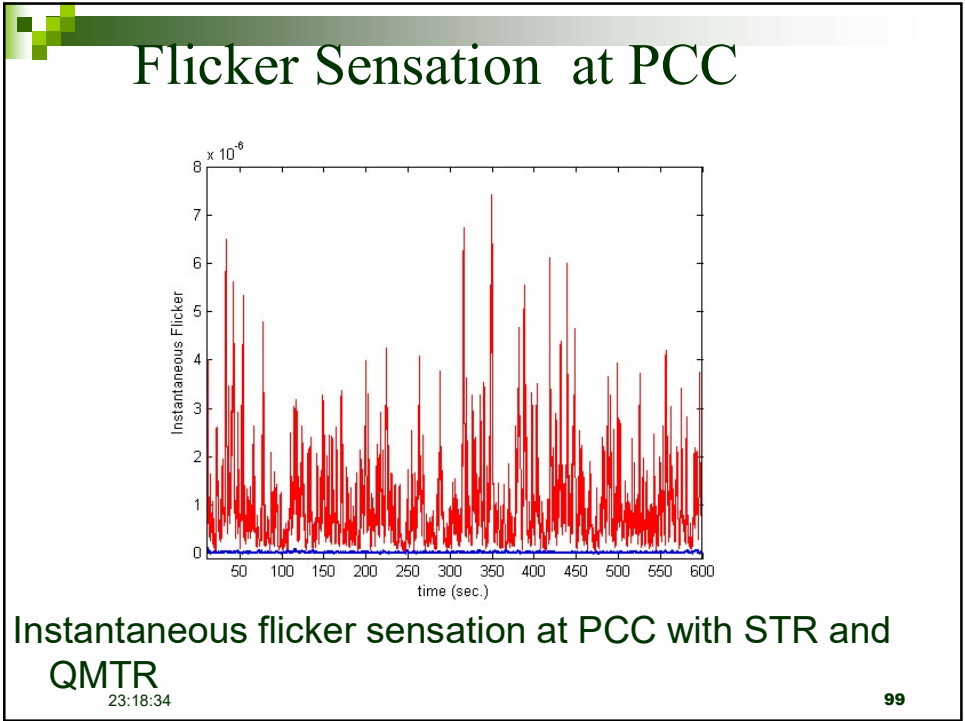
- Task 5: Averaging of variables (i.e. voltage and powers) at PCC using recorded data
- Task 6: Implementing the IEEE flickermeter to calculate the instantaneous flicker level sensation signal using recorded data

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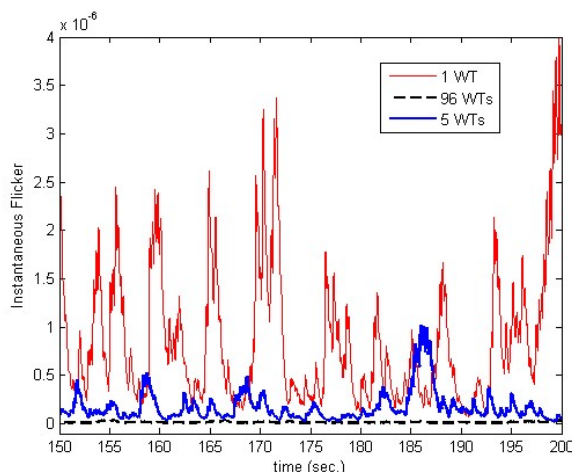
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Flicker Sensation at PCC



Instantaneous flicker sensation at PCC with different numbers of WTs

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References

- Natinal Resorces Canada www.canren.gc.ca
- The National Renewable Energy Laboratory (NREL) www.nrel.gov
- Danish Wind Industry Association www.windpower.org
- German Advisory Council on Global Change www.wbgu.de
- J. Manwell, J. McGowan, and A. Rogers, Wind Energy Explained - Theory Design and Application. John Wiley and Sons Ltd, 2002.
- E. Muljadi, C. Butterfield, J. Chacon, and H. Romanowitz, "Power quality aspects in a wind power plant," in IEEE Power Engineering Society General Meeting, Montreal, Quebec, Canada, June 2006
- J. M. Jonkman and M. L. J. Buhl, "Fast user's guide, www.nrel.gov," Aug. 2005
- E. Muljadi, C. Butterfield, A. Ellis, J. Mechenbier, J. Hochheimer, R. Young, N. Miller, R. Delmerico, R. Zavadil, and J. Smith, "Equivalentencing the collector system of a large wind power plant," in IEEE Power Engineering Society General Meeting, Montreal, Quebec

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